

Mark schemes

1.

(a) difference amplifier ✓

1

(b)  $V_{out} = (V_+ - V_-) \times (R_f / R_{in})$

$V_{out} = (0 \text{ V} - 150 \text{ mV}) \times (1 \text{ M}\Omega / 100 \text{ k}\Omega)$  ✓

$V_{out} = -1.5 \text{ V}$  ✓

1 mark for the correct resistor substitution / resistor ratio (10)

1 mark for -1.5 V (must have correct sign)

2

(c) Signal 2 is subtracted from signal 1 by the difference amplifier ✓

Noise is common to both so will be reduced / eliminated when subtracted ✓

Signals will also be subtracted resulting in an addition (re-enforcement) of the signal.

✓

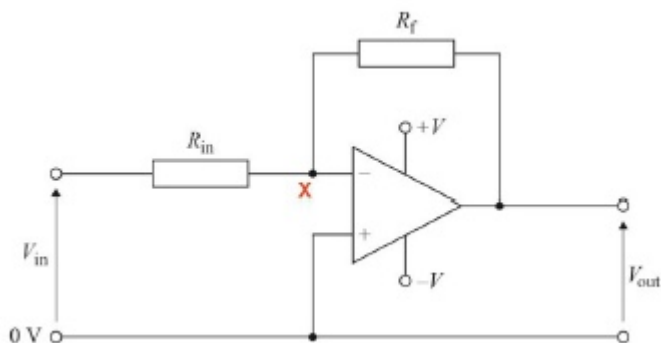
Accept arguments based on the 'phase' relationship

3

[6]

2.

(a)



Correct position of X:

1

(b) The non-inverting input

(non-inverting)

1

(c)  $I = (V_{in} - V_x) / R_{in} = (V_x - V_{out}) / R_f$

But  $V_x = 0 \text{ V}$  (a virtual earth)

$I = V_{in} / R_{in} = -V_{out} / R_f$

Making use of:  $I_{in} = -I_f$

$$\frac{V_{out}}{V_{in}} = \frac{R_f}{R_{in}}$$

Making use of virtual earth concept

2

(d) Voltage gain (Channel 1) =  $- R_f / R_{in}$  1

$-(150 \text{ k}\Omega / 7.5 \text{ k}\Omega)$

$-20$

*Both number **and** sign must be correct*

1

(e)  $V_{out} = - R_f (V_{in \text{ Ch1}} / R_1 + V_{in \text{ Ch2}} / R_2)$

$= - 150 \text{ k}\Omega (( 15\text{mV} / 7.5\text{k}\Omega) + (-100 \text{ mV} / 30 \text{ k}\Omega))$

$= - ((0.3) + (-0.5)) = 0.2 \text{ Volts}$

*Evidence of correct method*

*Answer **and** correct sign*

1

(f) By using variable resistors

The gain can easily be changed

**or**

the relative levels of the two channels can be set

**or**

the required balance between the two signals can be made

*One relevant point made*

1

[6]

3.

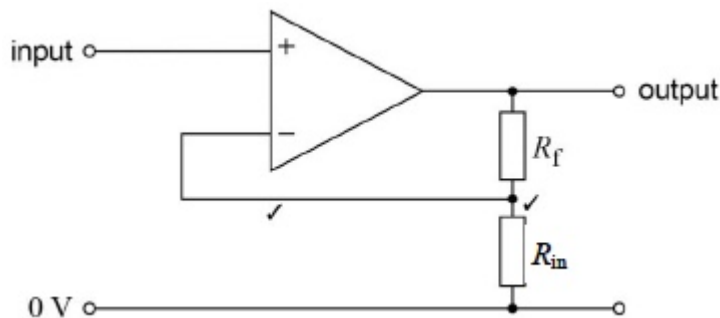
(a) Voltage in = Voltage out / Voltage gain

$= 3 \text{ V} / 40$

$= 75 \times 10^{-3} \text{ V} \checkmark$

1

(b)



*Two resistor chain, correctly labelled connected between output and ground*

*Inverting input connected to mid-point of resistor chain*

2

$$(c) \quad \frac{V_{out}}{V_{in}} = 1 + \frac{R_f}{R_{in}}$$

$$40 = 1 + \frac{R_f}{R_{in}} \quad \text{calculation to give resistor ratio of 39 } \checkmark$$

$$R_{in} = 1 \text{ k}\Omega ; R_f = 39 \text{ k}\Omega \checkmark$$

2

- (d) Desired gain  $\times$  bandwidth is  $40 \times 50 \text{ kHz} = 2 \text{ MHz} \checkmark$

The Op Amp can only provide  $\frac{1}{2}$  the amplification needed. Not suitable.  $\checkmark$

*1 mark - relevant calculation*

*1 mark - reference to only providing  $\frac{1}{2}$  require amplification / gain so not suitable*

2

[7]

4.

- (a) Photoconductive mode

*Accept 'reverse bias'*

1

- (b) Dark currents will become a source of noise – need to keep S:N as high as possible  
OWTTE

OR

Need to have a large difference in signal when detector is in light and dark  $\checkmark$

*Must include idea of 'noise'*

OR

*Must include concept of large signal change to represent digital signal*

1

- (c) At 850 nm,  $R_\lambda = 0.50 \text{ A/W} \checkmark$

*Reading from graph*

*Allow 0.49 A/W to 0.51 A/W*

$$\text{Using } R_\lambda = \frac{I_p}{P} \quad I_p = R_\lambda \times P \quad 0.50 \times 4 \times 10^{-6} = 2 \text{ }\mu\text{A} \checkmark \text{ ecf}$$

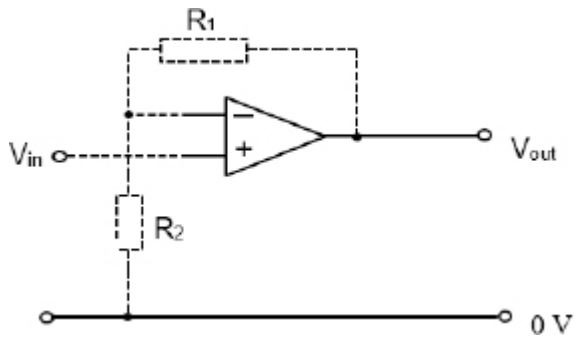
$$V_{out} = I_p \times R \quad 2 \text{ }\mu\text{A} \times 560 \text{ k}\Omega = +1.12 \text{ V} \checkmark$$

*Accept voltage in range of 1.10 V to 1.14 V*

*Accept value without + sign*

3

(d)



Correct configuration of  $R_1$  and  $R_2$  ✓

$R_1 : R_2$  ratio 3 : 1 in suggested range ✓

Label the input point which must have a direct connection to the non-inverting input ✓

One mark only

An inverting op amp configuration with a voltage gain  $-4$ .

3

[8]